

Missile Aerodynamics

- A brief discussion of aerodynamics is needed in order to appreciate the complexity of weapon system design
 - We're not planning to build a missile, but...
 - We need to understand basic aerodynamic principles in order to design a weapon system
- The aerodynamic building blocks to be discussed include
 - Basic aerodynamic principles (forces and moments)
 - Missile body type characteristics
 - Projectile stability
- These building blocks will be referenced in other lectures as we discuss numerous topics
 - Guidance law development
 - Weapon system design
 - Track processing (track filtering)
- First, some basic terms used in aerodynamics must be discussed

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- Speed can be measured using the speed of sound as a base scale
- This measurement of speed is referred to as Mach (M)

$$M = \frac{V_{\text{Mach}}}{V_{\text{sound}}}$$
- Mach number represents the ratio of ordered energy to random energy
- All aerodynamic coefficients are affected by the Mach number.
 - Variations with Mach number become more apparent as $M > 1$
- Sound travels at 1116 ft/sec at sea level
 - The speed of sound varies as a function of ambient temperature

$$V_{\text{sound}} \cong 49 \sqrt{T_{\text{amb}}}$$

* T_{amb} is temperature in Rankine [538.7° at sea level]

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- Streamlines define how air flows past the body as the body cuts through the atmosphere
- Streamlines differ as the speed in which air flows past the body increases
 - Four regions of missile speed
 - Subsonic ($Mach < 1.0$)
 - Transonic ($Mach \sim 1.0$)
 - Supersonic ($1.0 < Mach < 5.0$)
 - Hypersonic ($Mach > 5.0$)
- Air flow patterns over specific geometric shapes (correlating to specific missile parts) are dependent upon the regions listed above

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- Q is defined as

$$Q = \frac{\rho}{2} V^2 \cong (0.7)(P) M^2$$

This is the more common definition when $M > 0.5$
- Where
 - ρ is the ambient density (slugs/ft^3)
 - V is the missile velocity (ft/sec)
 - P is the ambient pressure (lbf/ft^2)
 - M is the Mach number
 - 0.7 is approximately one half the specific heat ratio of air
 - Q is a function of both speed and altitude

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- Pressure waves are the result of molecules of air being pushed together due to a body forcing its way through the atmosphere
- Pressure waves travel at the speed of sound (Mach 1)
- They travel in all directions from the disturbance
 - Similar to waves in a pool after throwing a rock in the water
 - As the speed of the flying body increases, the shape of the pressure circles change

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The Next Slide Illustrates Pressure Waves for Various Missile Speeds

Rowan University Pressure Waves

Rowan University Radome/Seeker

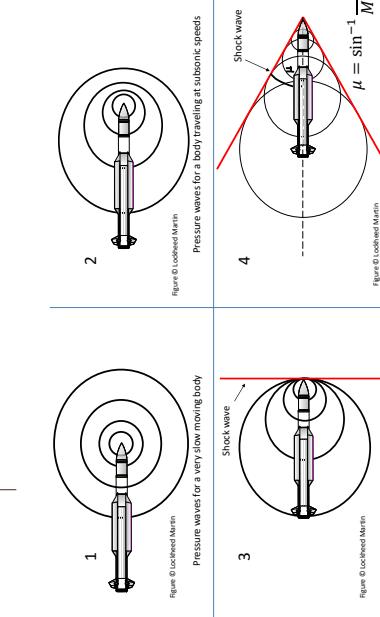


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Rowan University Angle of Attack

Important Terms in Missile Engineering

- ❑ Angle of attack (α) is the angle between the missile body center line (M_{C_L}) and the velocity vector of the missile.
 - Also referred to as the angle between the missile body axis and the wind axis.
- ❑ Angle of attack
 - Increases drag on the missile (more missile body is exposed)
 - Angle of attack is required for a missile to change direction

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Rowan University Forces and Moments

- ❑ Forces and Moments are defined in a body axis reference system
 - N – normal force (force perpendicular to the body axis)
 - Y – side force (force perpendicular to the body axis)
 - A – axial force (force along body axis, thrust and drag)
 - m – pitching moment about the lateral axis
 - n – yawing moment about the normal axis
 - l – rolling moment about the center line axis

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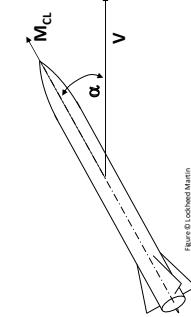


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Rowan University Forces and Moments

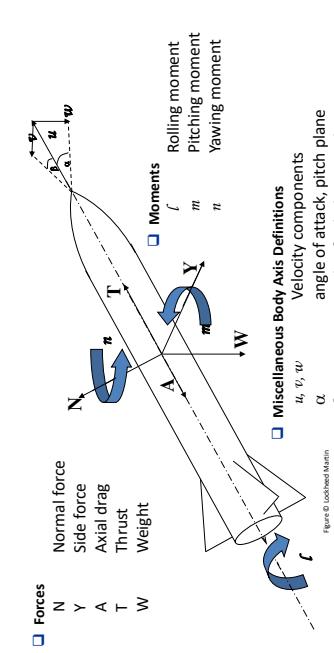


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Rowan University Force Coefficients

- ❑ Force coefficients:
$$C_N = \frac{N}{Q S_{Ref}}$$
$$C_Y = \frac{Y}{Q S_{Ref}}$$
$$C_A = \frac{A}{Q S_{Ref}}$$
Where:
 S_{Ref} is the reference area
 - ❑ For missiles, S_{Ref} is usually considered to be the maximum cross-sectional area
 - Compute the reference area using the diameter of the missile (cross sectional area)
- ❑ For airplanes, S_{Ref} is defined by the area of the wing

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Rowan University | Moment Coefficients

- ☐ Moment coefficients:

$$C_m = \frac{m}{Q S_{Ref} L_{Ref}} \quad C_n = \frac{n}{Q S_{Ref} r_{Ref}} \quad C_l = \frac{l}{Q S_{Ref} t_{Ref}}$$

S_{Ref} is the reference area (max. body cross sectional area)

L_{Ref}
For missiles, L_{Ref} is a reference length, or body diameter (more on this later)

For airplanes, L_{Ref} is related to the wing chord

Moment coefficients are taken about a reference center of gravity

Center of gravity changes as fuel/propellent is burned off

i.e. the interceptor rotates about its center of gravity due to a non-zero moment

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Rowan University | Force and Moment Coefficients Specific Properties

- ☐ C_N and C_m are proportional to the angle of attack (α)
 - Influenced by β
- ☐ C_r and C_a are proportional to the side-slip angle (β)
 - Influenced by α
- ☐ C_a is independent of both α and β
- ☐ C_l is dependent upon both α and β

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Rowan University | Force and Moment Coefficients Generic Properties

- ☐ Coefficients vary as a function of
 - Mach (M)
 - Angle of attack (α)
 - Sideslip (β)
 - Roll (ϕ)
- ☐ Coefficients are determined by theoretical design as well as wind tunnel test analysis
- ☐ Coefficients are referred to as proportionality factors
- ☐ Scalability
 - Makes wind tunnel work with models very effective
 - Aerodynamic forces scale by L^2 for similar configurations
 - Aerodynamic moments scale by L^3 for similar configurations

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Rowan University | Force and Moment Coefficients Specific Properties

- ☐ Axial drag (A) is far more sensitive to Mach than the normal force (N) or side force (Y)
 - ☐ Normal force is nearly independent of Mach
 - Provided the wings are slender and pointed
 - Low aspect ratio (delta shape)
 - ☐ Coefficients associated with the missile's rotational rates
 - Very complex
 - Burdensome to compute
 - They are not covered in this discussion

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Rowan University | Force and Moment Coefficients C_A (or C_N)

- ☐ A typical C_N vs. α plot at various Mach numbers would look like this:
- ☐ For each Mach number, C_N as a function of α is nearly linear for small α
 - ☐ This allows us to write the following:

$$C_N = \left(\frac{\partial C_N}{\partial \alpha} \right)_M \alpha$$

This means that each C_N is linear as a function of Mach

One can see that to get a good first order approximation, one could assume an average Mach resulting in

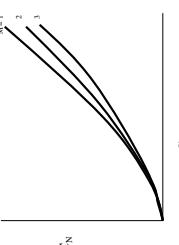
$$C_{N_{avg}} = \left(\frac{\partial C_N}{\partial \alpha} \right)_M$$

$$C_N \cong C_{N_{avg}} \alpha$$

Rowan University | Force and Moment Coefficients C_A

- ☐ A typical C_A vs. M plot would look like this:
- ☐ Since C_A is not very easy to describe as a function of M , we often express it in this manner

- ☐ A typical C_A vs. Mach plot would look like this:



$C_N \cong C_{N_{avg}} \alpha$

$C_A = Y_{Uckl}$

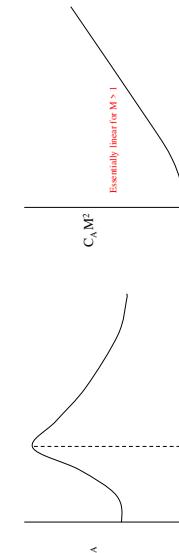
$C_A M^2 \cong C_1 M + C_2 M^2$ or $C_A \cong \frac{C_1}{M} + C_2$

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Rowan University | Force and Moment Coefficients C_A

- ☐ A typical C_A vs. M plot would look like this:
- ☐ Since C_A is not very easy to describe as a function of M , we often express it in this manner



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Rowan University | Induced Drag

- ❑ The induced drag (C_d) is the component of lift that resists missile motion
- ❑ It is the penalty one must pay to generate lift force on the missile
- ❑ The maneuvering efficiency (per G) is a function of induced drag

$$C_d = C_N \alpha = (C_N \alpha)^2$$

- ❑ One can represent maneuver G's as

$$\frac{n_z}{\alpha} = \frac{N}{w} = (C_N \alpha)^2 \frac{\alpha Q S_{ref}}{w}$$

- ❑ Therefore

$$\frac{n_z}{\alpha} = (C_N \alpha)^2 \frac{Q S_{ref}}{w}$$

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Rowan University | Lift and Drag Forces

- ❑ Normal and axial forces translate into lift and drag forces
 - Lift force is perpendicular to the velocity vector
 - Drag force is along the velocity vector
 - Sometimes it is desired to have the forces defined by the orientation of the missile velocity vector rather than the missile center line
- ❑ There is no lift without drag
 - It is a basic property of aerodynamics

Lift and Drag Terms

- ❑ We can simplify this to

$$L \cong N$$

$$D \cong A + N \alpha$$

- ❑ Lift and Drag can be normalized in the same manner as the Normal and Axial forces

$$C_L \cong C_N$$

$$C_D \cong C_A + C_N \alpha$$

- ❑ We can further simplify this to
- Zero-lift drag
- Induced drag, C_{D_I}

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Rowan University | Induced Drag

- ❑ Induced drag is the penalty paid for a change of direction by the missile
- ❑ It can be expressed as a function of the square of the acceleration.

$$C_{D_I} = \frac{n_z^2 w^2}{(C_N \alpha)^2 S_{ref}^2}$$

- ❑ Note which factors contribute to high induced drag, and which contribute to low induced drag
- ❑ The objective of a guidance law is for the missile to hit the target with the greatest amount of kinetic energy (velocity) possible
 - When developing a guidance law, the goal is to minimize the integral of the commanded acceleration over the time of flight as it should also reduce the induced drag
 - i.e.

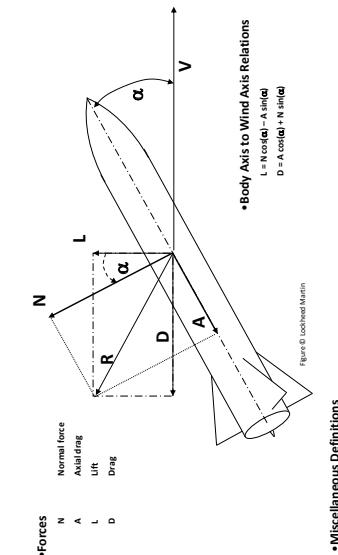
$$I = \int_0^T n_z^2 dt$$

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Rowan University | Comparing Forces

Lift and Drag vs Normal and Axial



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•Miscellaneous Definitions
velocity vector
angle of attack, pitch plane

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Rowan University | Computing Lift and Drag

- ❑ Lift and drag forces describe the forces acting on the missile in a plane defined by the missile velocity vector and the directions orthogonal to it
- ❑ The Normal and Axial forces can be defined as Lift and Drag terms as follows:

$$L = N \cos(\alpha) - A \sin(\alpha)$$

$$D = A \cos(\alpha) + N \sin(\alpha)$$

- ❑ Lift and Drag can be normalized in the same manner as the Normal and Axial forces

$$C_L \cong C_N$$

$$C_D \cong C_A + C_N \alpha$$

- Zero-lift drag
- Induced drag, C_{D_I}

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Rowan University | Static Margin

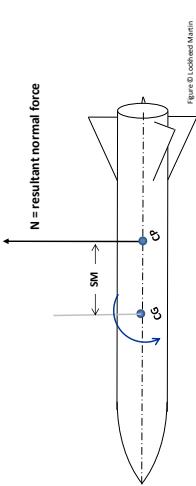
- ❑ The missile must be designed for stability during flight
 - Forces and moments acting upon the interceptor can easily result in an unstable flying configuration
 - One of the key concepts in understanding stable flight is static margin
- ❑ Static Margin is defined as the distance the center of gravity is aft of the center of pressure
 - $SM = CG - CP$
 - The interceptor is unstable when $SM > 0$
 - CG must be forward of CP
 - Rule of thumb: $SM \cong -0.50 d$ (50% of the missile diameter)
- ❑ Center of Pressure is the centroid of the longitudinal normal force distribution
 - Shifts due as a function of Mach and angle of attack
 - Shifts can be minimized using long slender wings
- ❑ Center of Gravity is the centroid of the gravitational forces acting on a body
 - Shifts as a function of propellant burn off

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Rowan University | Static Margin

- In a stable configuration ($SM < 0$), the static margin is directly related to a resultant moment about CG
- $m = N \cdot (SM)$
- Controlling that resultant moment is critical to ensure stability is maintained
 - It does not have to be zero, just controlled



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Rowan University | Deriving the Trim Condition

- Define the moments due to forces N and ΔM_t

$$m = N \cdot (SM) = \left(\frac{C_N}{\alpha}\right) \alpha Q S_{Ref} (SM)$$

$$\Delta m_t = \Delta N_t \cdot L_T$$

$$\Delta m_t = \left(\frac{C_N}{\delta}\right) (-\delta) Q S_{Ref} L_T$$
- Total moment about CG,

$$m_{CG} = m + \Delta m_t$$
- For trim, $m_{CG} = 0$,

$$0 = m + \Delta m_t$$
- The fin deflection required for trim conditions

$$\delta = \frac{(C_N/\alpha) \alpha (SM)}{(C_N/\delta) L_T}$$

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Rowan University | Missile Design Variation

- As a result, there is tremendous variation in missile design

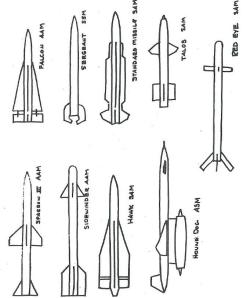


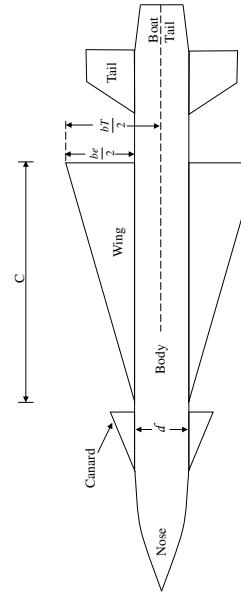
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The Missile Design Engineer's Optimum Design is Really the "Least Worst" Design

- Illustration of the major missile body parts that affect missile aerodynamics

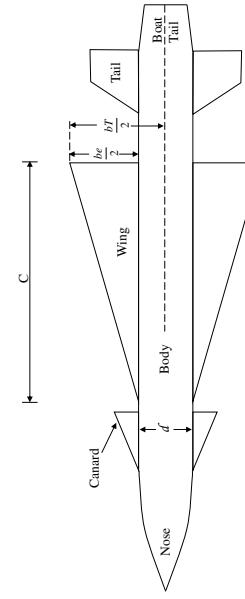


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Rowan University | Missile Body

- The final missile design is a compromise of the requirements and preferred approaches of the following design disciplines

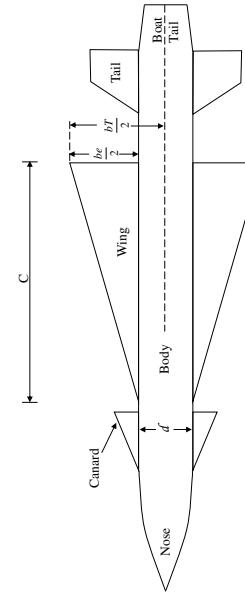


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Rowan University | External Missile Body

- Reflected upon the final design



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Rowan University | Trim Condition

- Refers to the condition at which the aerodynamic moments on the interceptor are balanced by the control surfaces
- The amount of tail deflection (δ) required to trim an interceptor is a function of SM and the tail control effectiveness, C_N/δ
- Tail deflection required for trim

$$\delta = \frac{(C_N/\alpha) \alpha SM}{(C_N/\delta) L_T}$$
 - Where:
 - L_T is the distance from the CG to the tail control surface
 - Since maximum tail deflection is fixed, a large static margin reduces the maximum trim angle of attack that can be achieved
 - Large static margin is very stable, but provides a sluggish interceptor response

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Rowan University | Missile Design Trade Space

- The missile designer must
 - Consider the aerodynamic configuration and estimate basic aerodynamic parameters
 - Determine the propulsion system requirements considering the mission requirements for range, speed, time-to-intercept and maneuverability
 - The final missile design is a compromise of the requirements and preferred approaches of the following design disciplines
- Aerodynamics
 - Propulsion
 - Structural design
 - Stability, Guidance and Control
 - Thermodynamics
 - Trajectory kinematics
 - Lethality (warhead - fuse)

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Rowan University | Airfoils

- One of the most important design decisions is body diameter
- There are very few drivers for having a small missile body diameter
 - Decreases drag
 - Launch platform capability
- There are many drivers for having a large missile body diameter
 - Increases seeker performance
 - Higher resolution
 - Lower noise
 - Increases blast fragmentation and warhead effectiveness
 - Larger diameter \rightarrow higher velocity fragments
 - Subsystem packaging (more room for your stuff)
 - Reduced CG travel and greater bending stiffness

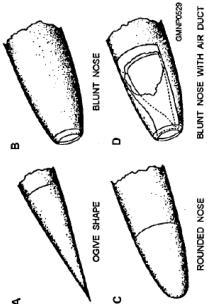
The Desire for a Low Drag Airframe Results in a Small Missile Body Diameter Despite All the Reasons for a Large Body Diameter

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Rowan University | Airfoils

- Nose shape requirements are driven by the presence of a seeker
- Missiles without a seeker can use a pointed nose cone
- Missiles with a seeker require a trade-off between low drag and good radome characteristics for accurate sensor measurements



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Rowan University | Airfoils

- Airfoils are the wings, fins, etc. that are attached to the missile body
 - Provide flight stability
 - Provide lift
 - Control the missile's flight path (movable surface)
- The traditional missile body has 3 potential control surfaces
 - Canard
 - Wing
 - Tail
- Taking advantage of the unique control surfaces of a missile allows one to
 - Create a robust guidance law
 - Design for optimal conditions
 - Improve performance

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Rowan University | Body

- Body fineness ratio (BFR) is the ratio of the missile length to the missile diameter
- $$BFR = \frac{\text{length}}{\text{diameter}}$$
- Typical range of the BFR is 5 to 25
 - Portable anti-armor missile have low BFR (Javelin)
 - Air-to-air missiles have high BFR (AMRAAM)
- Benefits of a large body diameter
 - Improved seeker and warhead effectiveness
 - Reduced CG movement during rocket motor burn
 - Greater bending stiffness
 - More internal volume
 - Reduced pitching and yawing inertia
- Benefits of a small body diameter
 - Missile drag

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Rowan University | Nose Fineness Ratio

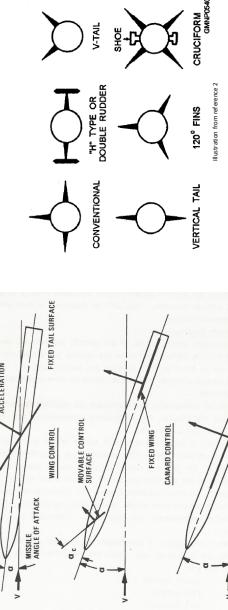
- Nose fineness ratio (NFR) is the ratio of the nose length to the max. nose diameter
- $$NFR = \frac{\text{length}}{\text{diameter}}$$
- Benefits of a high NFR (~5)
 - Excellent aerodynamics
 - Low observables
 - Reduces wave drag
- Benefits of a low NFR (<0.5)
 - Minimal radome slope errors
- Typical range of the NFR is 2 to 4 for supersonic missiles

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Rowan University | Airfoils

- View from Aft

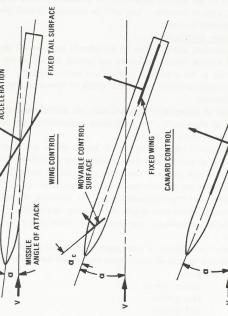


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Rowan University | Control Surfaces

- View from Side



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Rowan University | Body Fineness Ratio

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 - Missile drag

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Rowan University | Nose Fineness Ratio

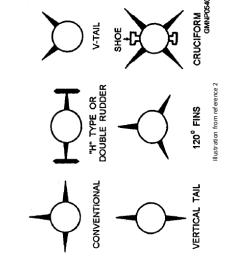
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- View from Aft

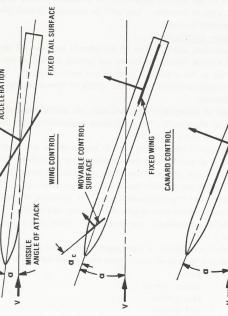


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Rowan University | Airfoils

- View from Side



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Rowan University | Control Surface Characteristics



Control Surface Requirements

Control Type	Characteristics	Pro	Con
Wing	Low angle of attack during the maneuver	<ul style="list-style-type: none">Desirable for air breathing engines because the engine may cause the engine to stall	<ul style="list-style-type: none">Significant structural weightLarge actuation system needed to move the wing
Canard	Lower α than tail, higher than wing	<ul style="list-style-type: none">Limited to max $\alpha = 45^\circ$Physical location is where guidance equipment is normally located	<ul style="list-style-type: none">Limited a capability due to control surface saturation$\alpha_{canard} = \delta_{canard} + \alpha_{body}$
Tail	Vector force produced by control surface is opposite of the desired maneuver	<ul style="list-style-type: none">High α capabilityLift produced by wing and body must overcome tail force to achieve desired acceleration	<ul style="list-style-type: none">$\alpha_{tail} = \delta_{tail} - \alpha_{body}$Good physical location (no competition)

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Rowan University | Additional Control Techniques



- Non-traditional means of controlling the missile flight are also common

- Thrust controllers

- Thrust Vector Actuator (TVA)

- Nozzles typically located at the rear of the missile which generate a directional thrust for the purpose of changing missile flight path only

- May be the main rocket motor or an auxiliary thrust for the flight path control only

- Thrust Vector Controller (TVC)

- Attitude control motors

- Vane inserted into (or just outside) of the rocket motor nozzle to deflect thrust
- Small explosives in the missile which are fired to generate a nearly instant change angle of attack, thus inducing an normal force

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01-01

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Rowan University | Missile Control Techniques Illustrated



- A missile's flight is controlled through the deflection of various missile surfaces

- Tail

- Wing

- Canard

- Additional means of controlling flight are also possible

- Thrust Vector Actuator – jets located near the tail of the missile (TVA)

- Thrust Vector Control – surface which deflects the thrust of the rocket motor (TVC)

- Attitude control motors (ACM)

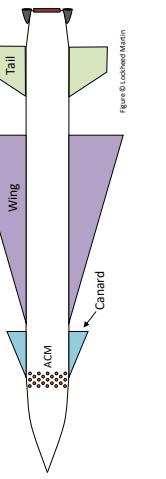


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Rowan University | Wing Size



- Benefits of small or no wings
 - Increased range in high supersonic flight, high dynamic pressure
 - Provides better stability and control at high angles of attack
 - Lower radar cross section (RCS)
 - Launch platform compatibility (packaging, storage)
- Benefits of larger wings
 - Increased range in subsonic flight / low dynamic pressure
 - Lower guidance time constant (more maneuverable)
 - More capability at higher altitudes
 - Less seeker error due to dome error slope (lower angle of attack)
 - Lower gimbal requirements for seeker

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